Project Name: Proposed Office Development at Caroline Hill Road, Causeway Bay
Daily Water Demand Calculation

## Calculation of Peak Daily Demand

## 1. AC Make-up Water

> As per CT1A,

Estimated peak daily make-up water demand by T1T2 cooling tower $=843.02 \mathrm{~m}^{3} /$ day

> As per CT1A,

Estimated peak daily make-up water demand by T3 cooling tower $=21.36 \mathrm{~m}^{3} / \mathrm{day}$
Total peak daily make-up water demand of CHR $\quad=864.38 \mathrm{~m}^{3} /$ day
2. Water Consumption Estimation for Proposed Development
(Based on EPD Guidelines for Estimating Sewage Flows for Sewage Infrastructure Planning)

## Design Assumption:

Global Unit Flow Factors as per Tables T-2 and T-3
Catchment Inflow Factor for Wan Chai (PCIF =1.0) as per Table T-4

| Estim | Water Consumption for Caroline Hill Road | Estimation |
| :---: | :---: | :---: |
| (1) | GFA (m²) for Office use | 85,300 |
| (2) | Assumed 60\% for Usable Floor Area | 51,180 |
| (3) | Worker Density (No. of Worker per 100m²) | 3.2 |
| (4) | No. of Employee | 1,638 |
| (5) | Unit flow factor ( $\mathrm{m}^{3} /$ person/day) - J6 Financial, Insurance, Real Estate \& Business Services | 0.08 |
| (6) | Sub-total Daily Water Consumption ( $\mathrm{m}^{3} /$ day) | 131.0 |
| (7) | GFA ( $\mathrm{m}^{2}$ ) for Non Domestic | 10,000 |
| (8) | Assumed 60\% for Usable Floor Area | 6,000 |
| (9) | 50\% GFA ( $\mathrm{m}^{2}$ ) for F\&B | 3,000 |
| (10) | Worker Density (No. of Worker per $100 \mathrm{~m}^{2}$ ) | 5.1 |
| (11) | No. of Employee | 153 |
| (12) | Unit flow factor (m³/person/day) - J10 Restaurant \& Hotels | 1.58 |
| (13) | Sub-total Daily Water Consumption ( $\mathrm{m}^{3} /$ day $)$ | 241.7 |
| (14) | $50 \%$ GFA ( $\mathrm{m}^{2}$ ) for Retail | 3,000 |
| (15) | Worker Density (No. of Worker per $100 \mathrm{~m}^{2}$ ) | 2.1 |
| (16) | No. of Employee | 63 |
| (17) | Unit flow factor (m³/person/day) - J4 Wholesale \& Retail | 0.28 |
| (18) | Sub-total Daily Water Consumption ( $\mathrm{m}^{3} /$ day $)$ | 17.6 |
| (19) | GFA (m) for GIC | 3,100 |
| (20) | Assumed 60\% for Usable Floor Area | 1,860 |
| (21) | Worker Density (No. of Worker per 100m²) | 2.3 |
| (22) | No. of Employee | 43 |
| (23) | Unit flow factor ( $\mathrm{m}^{3} /$ person/day) - J11 Community, Social \& Personal Services | 0.28 |
| (24) | Sub-total Daily Water Consumption ( $\mathrm{m}^{3} /$ day) | 12.0 |
| (25) | Total Daily Water Consumption (6)+(13)+(18)+(24), (m²/day) | 402.4 |

## 3.Total Water Consumption Estimation for Proposed Development



## Calculation of Pipe Capacity

DN150 Water PE Pipe Capacity

| Nominal <br> Diameter <br> $(\mathrm{mm})$ | Internal <br> Diameter <br> $(\mathrm{mm})$ | Pipe <br> Material |
| :---: | :---: | :---: |
| 200 | 200 | DI |
| 150 | 147 | PE100 <br> (OD180) |


| Q | $=\mathrm{AV}$ |
| ---: | :--- |
| DN150 Water Pipe Capacity | $=\pi(0.0736)^{2}(1.5)$ |
| (Assume $1.5 \mathrm{~m} / \mathrm{s})$ | $=0.0255 \mathrm{~m}^{3} / \mathrm{s}$ |
|  | $=2205.52 \mathrm{~m}^{3} / \mathrm{d}$ |
|  |  |
| DN150 Water Pipe Capacity | $=\pi(0.0736)^{2}(2.0)$ |
| (Assume $2.0 \mathrm{~m} / \mathrm{s})$ | $=0.0340 \mathrm{~m}^{3} / \mathrm{s}$ |
|  | $=2940.69 \mathrm{~m}^{3} / \mathrm{d}$ |

DN200 Water Ductile Iron Pipe Capacity

| $Q$ | $=A V$ |
| ---: | :--- |
| $\varnothing 200$ Water Pipe Capacity | $=\pi(0.100)^{2}(1.5)$ |
| $($ Assume $1.5 \mathrm{~m} / \mathrm{s})$ | $=0.0471 \mathrm{~m}^{3} / \mathrm{s}$ |
|  | $=4071.50 \mathrm{~m}^{3} / \mathrm{d}$ |
| $\varnothing 150$ Water Pipe Capacity | $=\pi(0.100)^{2}(2.0)$ |
| (Assume $2.0 \mathrm{~m} / \mathrm{s})$ | $=0.0628 \mathrm{~m}^{3} / \mathrm{s}$ |
|  | $=5428.67 \mathrm{~m}^{3} / \mathrm{d}$ |
|  |  |
|  | DN150 Water pipe is enough for the whole CHR development |$\quad$| as per WSD DI1309 requirement |
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